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⑯ Rollers with oriented fibre reinforcement and method of making them.

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Courier Press, Leamington Spa, England.

Description

This invention relates to rollers with elastomeric outer surface layers for tractional driving of loads, for example, cargo rollers for use in aircraft cargo holds, and to methods of making such rollers.

Rubber rollers are used in a variety of conveyor transport systems to move freight from one location to another. Such systems typically use a number of rubber rollers extending slightly above the transport surface and powered by electric motors to move freight from one end of the transport surface to the other. One of the most demanding applications of rubber rollers is that of cargo rollers in the cargo hold of an aircraft.

Cargo rollers in the cargo bay of an aircraft are required to be capable of moving heavy loads quickly and efficiently. Such cargo rollers must have a high surface coefficient of friction to prevent slippage when cargo contacts the roller, thereby resulting in the cargo roller going from no load to full load, for example from zero to 500 pounds, virtually instantaneously.

The result of such severe load requirements is that rollers in the cargo bay of aircraft have had a relatively short life in the past, with the surface of the rubber roller degrading and wearing down relatively quickly, requiring expensive and time-consuming replacement of the rubber rollers in the aircraft cargo bay. Since a typical passenger aircraft has about 40 rollers per aircraft, and a typical cargo aircraft has about 80 rollers per aircraft, it may be appreciated that frequent replacement of the rollers in the cargo bay has been a major maintenance problem.

One possible solution to premature cargo roller wear is to use a harder rubber compound. Unfortunately, this has adverse effects in that the surface coefficient of friction is substantially reduced as rubber hardness is increased, resulting in unsatisfactory performance of the harder rubber rollers. In addition, another problem experienced using different rubber formulations is chunking, where chunks of the rubber portion of the cargo roller break off resulting in dynamic destruction of the cargo roller in a random and unpredictable manner. Thus, it is apparent that reformulation of the rubber compound used in manufacturing the rollers is not the solution to the problem of premature wear in cargo rollers.

In addition, several other factors exist in the design of rollers for aircraft cargo bays. It is desirable that the rubber compound used have not only good abrasion resistance and tear resistance, but that it have good weather and oil resistance as well. Since the temperature range at which aircraft cargo bays may be loaded or unloaded may include fairly cold temperatures i.e. temperatures in the -28.9° to -40°C (-20° to -40°F) region, as well as storage temperatures of up to 73.89°C (165°F), the rollers must be usable over a fairly wide temperature range. Finally, since the rollers are to be used on-board aircraft, it is desirable that the rubber compound used

have at least some degree of resistance to flammability. In short there has been a particularly strong demand by airlines for the development of a cargo bay roller with not only good performance characteristics, but also a high degree of resistance to wear resulting in an extended operating life of the rollers.

Document FR-A-2242874, which corresponds to the pre-characterising portion of claim 1, teaches inclusion of short fibres parallel to the axis in a rubber roller.

The premature wear problems associated with the use of rubber rollers in aircraft cargo bays are solved by the present invention through the incorporation of specifically oriented fibre strands into the elastomer used in manufacturing the cargo roller. The fibre strands are orientated circumferentially with respect to the hub ground whose exterior the outer elastomeric layer is applied. The present invention allows the use of a rubber compound having desirable physical characteristics and requires only a single additional step to incorporate the chopped fibre strands into the rubber.

Thus, according to the present invention from one aspect, a roller for tractional driving of loads comprises a cylindrical hub adapted to be driven and an elastomeric surface layer fixedly installed on said cylindrical hub for tractional contact with the loads, characterised in that said elastomeric surface layer contains fibre strands dispersed therein only in substantially circumferential orientation around said cylindrical hub.

Preferably the fibre strands are not greater in length than 12.7mm (half an inch); for example they may comprise chopped fibre strands of between 4.76mm and 12.7mm (three-sixteenths of an inch and half an inch) in length. The material of the fibre strands may advantageously be an aromatic polyamide, for example Kevlar or Nomex, or a polyethylene terephthalate, for example, Dacron, although other natural or synthetic fibres could be used. The fibres may comprise between 0.5% and 3% of the weight of the elastomer in the elastomeric surface layer.

The elastomeric surface layer may be of neoprene, nitrile or urethane, and may have an original hardness of between 60 and 70 on the ASTM D 2240 type A durometer scale, which is raised to between 70 and 75 on that scale by the dispersion therein of the fibre strands.

From another aspect, the invention comprises a traction roller drive system, comprising a housing, a roller having a cylindrical hub adapted to be rotatably driven and having an elastomeric surface layer extending over the cylindrical outer surface of the hub, the elastomeric surface layer incorporating a dispersion of circumferentially orientated fibre strands as discussed above, and the roller hub being mounted in the housing with the elastomeric surface layer extending in part above the level of the housing to provide a driving surface.

From yet another aspect, the present invention comprises a method of manufacturing a traction

roller, which comprises providing a cylindrical hub adapted to be rotatably driven; dispersing a plurality of lengths of fibre strands into an elastomeric compound with said fibre strands in substantially parallel orientation, and installing about said cylindrical hub a layer of said elastomeric compound with said dispersed fibre strands so the orientation of said fibre strands in said layer of elastomeric compound is substantially circumferential about said cylindrical hub.

From yet another aspect the present invention comprises a method of manufacturing a tractive driving roller characterised by the steps of incorporating chopped fibre strands into an uncured elastomeric compound with said chopped fibre strands in substantially parallel orientation forming at least one pad from said uncured elastomeric compound with said chopped fibre strands incorporated therein in said substantially parallel orientation in said pad, placing said pad around at least a portion of the circumference of a cylindrical hub with said chopped fibre strands in said pad in substantially circumferential orientation around said hub and applying heat and pressure to said pad around said hub in a curing press to cure said elastomeric compound.

In one form of the method of the invention, chopped fibre strands are incorporated into uncured rubber in a two roll rubber mill, which is commonly used to mix the rubber formula. By using the technique of the present invention, the chopped fibre strands are incorporated into the uncured rubber with the fibres in a substantially parallel orientation. Such parallel orientation of the fibres results in greatly superior rubber strength in the direction of fibre orientation. The reinforced uncured rubber is then cut to predetermined size and bonded to a metal roller hub in a curing press with the fibres in the rubber oriented in a circumferential direction about the metal roller hub.

The resulting rubber roller has been found to be substantially more wear-resistant than existing rubber rollers in aircraft cargo bay applications. In fact, a roller manufactured utilising the principles of the present invention has an expected lifetime greater than ten times the lifetime of previous non-reinforced rubber rollers. Other than the increased lifetime of the reinforced rubber roller, there are substantially no differences in operational characteristics of the reinforced rubber roller as compared to previous non-reinforced rubber rollers. Although the incorporation of chopped fibre strands increased the hardness of the rubber material by compensating in the formulation of the uncured rubber, the final hardness of the fibre-reinforced rubber roller may be made close enough to the hardness of the non-reinforced rubber roller to result in a substantially identical coefficient of friction and operational capability.

The cost of producing the fibre-reinforced rubber roller is only minimally greater than the cost of producing non-reinforced rubber rollers, since only a single additional step is required to intro-

duce the chopped fibre strands into the uncured rubber formula. The greatly increased life time of the fibre reinforced rubber rollers quickly compensates for the slight increase in cost in manufacture of the roller. Therefore, it may be appreciated that a fibre reinforced rubber roller constructed according to the present invention represents a substantial gain in the art at minimal cost, while providing the same high degree of performance required in applications as aircraft cargo bay rollers.

The invention may be carried into practice in various ways, but one specific embodiment thereof will now be described by way of example only and with reference to the accompanying drawings in which:-

FIGURE 1 illustrates the incorporation of chopped fibre strands into uncured rubber on a two roll rubber mill;

FIGURE 2 is an exploded perspective view of the manufacture of a fibre reinforced rubber roller in a curing press using the fibre reinforced rubber mixed on the two roll mill of FIGURE 1;

FIGURE 3 is a perspective view of the completed fibre reinforced rubber roller made in the curing press of FIGURE 2; and

FIGURE 4 shows the roller of FIGURE 3 mounted for operation in a motorised cargo roller assembly.

Rubber is typically blended by a rubber manufacturer to meet the performance requirements of the purchaser, and is supplied to the purchaser in uncured rough slabs typically weighing 5-100 pounds. Rubber for use in aircraft cargo rollers must have good weather resistance, oil resistance, and abrasion and tear resistance, as well as being at least somewhat burn-resistant. The elastomer used for roller applications is generally synthetic rubber, such as neoprene, nitrile, or urethane.

The rubber formulation includes other components often making up a substantial portion of the formulation. The rubber is formulated with the weight of the elastomer being designated as 100 parts, and the weight of other components being specified as percentage parts of the total weight of the elastomer used. Typically carbon black is added to give strength and a reinforcing effect to the compound, oil is added as an extender for the elastomer, and zinc oxide, stearic acid, and an accelerator are used to control the rate and degree of vulcanisation. Other components may be added to improve aging characteristics, reduce fatigue cracking, and to act to improve fire-retardant properties. The formulation of rubber for roller applications is thus well known in the art, and is done by rubber companies such as Goodyear, Firestone, and B. F. Goodrich.

Since under the present invention chopped fibre strands are to be added to the rubber, which will act to increase the hardness of the rubber, the rubber formula should be specified to have a hardness less than the desired final hardness of the rubber roller. For example, while rubber rollers without fibre reinforcement typically have

a hardness of between 70 and 75 on the ASTM D 2240 type A (hereinafter Type A) durometer scale, the rubber formula for use with chopped fibre strands may typically have a hardness of between 60 and 70 on the Type A Scale in the preferred embodiment.

As stated earlier, specially blended rubber is generally supplied in uncured slabs each weighing 5-100 pounds. The specially blended rubber 10 is fed into a two roll rubber mill 20 shown in FIGURE 1, having a faster steel roller 22 and a slower steel roller 24. Since the rollers 22, 24 rotate at different surface speeds towards each other, a high shear condition results that aids in the mixing of the rubber formulation 10. As the rubber 10 comes out of the bottom of the two roll mill 20, it is taken by the operator and reinserted into the two roll mill 20 between the rollers 22, 24, thus resulting in a continuous roller of rubber 10 around the faster roller 22, as shown in FIGURE 1. Since the rubber slab is sized to have slightly more rubber than needed to make a band around the faster roller 22, a portion of the rubber 10 will pile up in a rubber bank 30 atop and between the rollers 22, 24.

As the rubber 10 is run on the two roll mill 20, it will increase in temperature and become more pliable, a step which must be followed before the fibre may be incorporated into the rubber. Typically, the operator may cut or slash the rubber 10 around the roller 22, pull the rubber from the bottom of the roller 22 outwardly and reinsert it into the top of the two roll mill 20. This process is called "cutting from side-to-side", is well known in the art, and in fact is used by rubber manufacturers to mix the rubber formulation. Another technique used by manufacturers to mix the rubber is "cross-milling", which consists of cutting the rubber around the roller, rilling it up, and reintroducing it to the two roll mill end first, thusly milling the rubber in a direction perpendicular to the original direction. Crossmilling and cutting from side-to-side both may be used before fibre is added to the rubber, when the rubber is mill freshened.

The chopped fibre 40 to be incorporated into the rubber 10 is an aromatic polyamide such as Kevlar or Nomex or a polyethylene terephthalate such as Dacron in the preferred embodiment, with a fibre length from 4.76mm to 12.7 millimetres (three-sixteenths of an inch to one-half inch), with the amount of fibre to be incorporated measured as a percentage of the elastomer in the rubber formula. The diameter of the fibre typically may be from 0.019mm (0.00075 inch) to 0.127mm (0.005 inch). Polyamides such as nylon can also be used for the fibres as can natural fibres such as hemp or cotton. Kevlar, Nomex, or Dacron are preferred because of their superior fibre strength. Typically, from 0.5 to 3 parts of fibre per hundred parts of elastomer are used.

The length of the fibre must be at least 4.76mm (three-sixteenths of an inch) to provide sufficient reinforcement properties, and not greater than 12.7 mm (one-half inch) long since longer fibres

are hard to blend in. The amount of fibre incorporated in the rubber formula must be sufficient to provide adequate reinforcement and yet is limited by the hardness of the resulting fibre-reinforced rubber. For example, for rubber formulas having a hardness of between 60 and 70 on the Type A Scale, if greater than 3 parts of fibre per 100 parts of elastomer are added, the hardness of the resulting fibre-reinforced rubber will be too high, resulting in the roller having a low surface coefficient of friction and a tendency to slip. Typically, a final hardness of 75 on the Type A Scale is the upper limit of hardness for rubber rollers in aircraft cargo bay applications.

5 While the mill is running, the fibre strands 40 are sprinkled by the operator of the two roll mill 20 onto the rubber bank 30 which has built up on the faster roller 22. By then allowing the two roll mill 20 to run and shear the rubber 10, the fibres 40 will be dispersed in the rubber 10 with a substantially parallel orientation which is circumferential around the faster roll 22. It is very important to note that while cutting from side-to-side may be done after the fibre is added, cross-milling may not be done. The reason for not cross-milling is that if cross-milling is done after the fibre is added, the fibre orientation in the rubber will not be substantially parallel.

10 After the fibre 40 is incorporated in the rubber 10, the band of rubber 10 may be slashed and removed from the two roll mill 20. It may be noted that the thickness of the rubber 10 which is determined by the two roll mill 20, should be only slightly greater than the actual thickness needed for construction of the rubber roller.

15 The reinforced rubber is then cut into pre-formed pads 50 as shown in FIGURE 2, each of which will extend halfway around the completed rubber roller.

20 A metal roller hub 60 about which the rubber pads 50 will be placed may be coated with an adhesive to ensure that the rubber pads 50 will adhere to the hub 60. The rubber pads 50 and the hub 60 are then placed into the curing mould having a top half portion 70 and a bottom half portion 72, as shown in FIGURE 2. The curing mould uses a pressure varying from 4136.856 to 6894.76LPa (600 to 1000 psi), and a curing temperature of approximately 154°C (310°F) for about 35 minutes to cure the rubber. The completed rubber roller 80 shown in FIGURE 3, thus has a rubber covering with the fibres extending in a substantially circumferential orientation.

25 It is important to note that if the fibres in the roller 80 are not substantially circumferentially oriented, the roller 80 will not have superior wear resistance. In fact, if non-oriented fibres are used one of two results is inevitable: either so much fibre is used to obtain a sufficient degree of wear resistance that the hardness of the roller is so high that it will have virtually no gripping power at all, resulting in a totally useless roller, or there will be insufficient circumferential fibre orientation to increase wear resistance, resulting in a rubber roller which wears out too quickly.

The rubber roller 80 may then be inserted into a typical motorised drive unit 90 as shown in FIGURE 4. The motorised drive unit 90 is inserted into the cargo deck of the aircraft cargo bay, and the roller 80 may be operated either to load or unload cargo from the aircraft. It has been found that a cargo roller 80 constructed according to the principles of the present invention provides a useful life which is greater than ten times the useful life of a rubber roller not containing oriented fibre reinforcement. This substantial increase in the useful life of the rubber roller 80 is obtained at relatively minimal increased cost per roller, making the roller of the present invention a highly desirable product.

Thus, it may be appreciated that the rubber roller 80 of the present invention presents the advantage of greatly increased wear resistance and a dramatically extended lifetime at a minimal cost increase, while still presenting desirable physical characteristics. Weather resistance, oil resistance, and non-inflammability characteristics of a roller 80 constructed according to the principles of the present invention are generally at least as good as non-reinforced rubber rollers, and also result in reduced maintenance and replacement time by the aircraft operator. The present invention is therefore a substantial improvement in the art, while affording virtually no drawbacks.

Claims

1. A roller (80) for tractional driving of loads, comprising; a cylindrical hub (60) adapted to be driven, and an elastomeric surface layer (50) fixedly installed on said cylindrical hub for tractional contact with the loads, characterised in that said elastomeric surface layer (50) contains fibre strands (40) dispersed therein only in substantially circumferential orientation around said cylindrical hub (60).

2. A roller as defined in Claim 1 wherein said elastomeric surface layer (50) containing said fibres has a hardness not greater than 75 on the ASTM D 2240 type A durometer scale.

3. A roller as defined in Claim 1 or Claim 2 wherein said elastomeric surface layer (50) is formulated using an elastomer selected from the group consisting of neoprene, nitrile, and urethane.

4. A roller as defined in Claim 1 or Claim 2 or Claim 3 wherein elastomeric compound comprising said elastomeric surface layer (50) has a hardness between 60 and 70 on the ASTM D 2240 type A durometer scale.

5. A roller as defined in Claim 4 wherein the hardness of the elastomeric layer (50) is raised by the dispersion therein of said fibre strands (40) to between 70 and 75 on the ASTM D 2240 type A durometer scale.

6. A roller as defined in any one of Claims 1 to 5, wherein said fibre strands (40) are not greater than 12.7mm (one half inch) in length.

7. A roller as defined in Claim 6 wherein said

fibre strands (40) are chopped for fibre strands between 4.76 mm and 12.7mm three-sixteenths of an inch and one-half inch in length.

8. A roller as defined in any one of Claims 1 to 7 wherein said fibre strands (40) weigh between 0.5% and 3% of the weight of the elastomer in said elastomeric surface layer (50).

9. A roller as defined in any one of Claims 1 to 8 wherein the material of said fibre strands comprises an aromatic polyamide, for example, Kevlar or Nomex, or a polyethylene terephthalate, for example Dacron.

10. A roller as defined in any of the preceding claims in which said elastomeric surface layer (50) is bonded by adhesive to said cylindrical hub (60).

11. A roller as defined in any one of Claims 1 to 10 wherein said elastomeric layer (50) has been bonded to said hub (60) under heat and pressure to cure said elastomeric layer.

12. A traction roller drive system, comprising a housing (90), a roller (80) having a cylindrical hub (60) adapted to be rotatably driven and having an elastomeric surface layer (50) extending over the cylindrical outer surface of said cylindrical hub, the roller hub being mounted in the housing with said elastomeric surface layer extending in part above the level of said housing to provide a driving surface and means for selectively reversibly driving said cylindrical hub, characterised in that the elastomeric surface layer (50) of the roller is as defined in any one of Claims 1 to 11.

13. A method of manufacturing the tractional driving roller (80) claimed in any one of Claims 1 to 11 characterised by the steps of: incorporating chopped fibre strands (40) into an uncured elastomeric compound with said chopped fibre strands in substantially parallel orientation; forming at least one pad (50) from said uncured elastomeric compound with said chopped fibre strands (40) incorporated therein in said substantially parallel orientation in said pad; placing said pad (50) around at least a portion of the circumference of a cylindrical hub (60) with said chopped fibre strands (40) in said pad in substantially circumferential orientation around said hub; and applying heat and pressure to said pad (50) around said hub (60) in a curing press (70, 72) to cure said elastomeric compound.

14. A method as defined in Claim 13 wherein said incorporating step comprises: running said uncured elastomeric compound on a two roller mill (20); sprinkling said chopped fibre strands (40) onto said uncured elastomeric compound as it is running on said two roller mill (20) said chopped fibre strands thereby becoming incorporated into said uncured elastomeric compound with said substantially parallel orientation.

15. A method as defined in Claim 13 or Claim 14 wherein said forming step comprises: rolling said uncured elastomeric compound with said chopped fibres (40) incorporated therein to a preselected thickness; and cutting said uncured elastomeric compound with said chopped fibres (40) incorporated therein to a preselected thickness; and cutting said uncured elastomeric com-

pound with said chopped fibres (40) incorporated therein to a predetermined size.

16. A method as claimed in any one of Claims 13 to 15, wherein a plurality of said pads (50) are formed and placed around said hub (60) to cover the entire circumference of said hub, each of said pads being placed so said chopped fibres (40) therein are oriented in said substantially circumferential orientation around said hub (60).

17. A method as defined in any one of Claims 13 to 16, wherein said application of heat and pressure step comprises the application of a pressure of from 4136.856 to 6894.76 KPa (600 to 1000 psi) at approximately 154°C (310°F) for about 35 minutes.

18. A method as defined in Claim 17 including the additional step of applying an adhesive to said hub (60) before said pad is placed around said hub.

19. A method of manufacturing a frictional driving roller characterised by the steps of: providing a cylindrical hub (60) adapted to be rotatably driven; dispersing a plurality of lengths of fibre strands (40) into an elastomeric compound with said fibre strands only in substantially parallel orientation; and installing about said cylindrical hub (60) a layer (50) of said elastomeric compound with said dispersed fibre strands (40) so the orientation of said fibre strands in said layer of elastomeric compound is substantially circumferential about said cylindrical hub.

Patentansprüche

1. Walze (80) für den Zugantrieb von Belastungen, mit einer zylindrischen Nabe (60), die antreibbar ist, und einem elastomeren Oberflächenbelag (50), der auf der zylindrischen Nabe für den Zugkontakt mit den Belastungen fest aufgebracht ist, dadurch gekennzeichnet, daß der elastomere Oberflächenbelag (50) Faserstränge (40) aufweist, die darin nur in im wesentlichen in Umfangsrichtung verlaufender Orientierung um die zylindrische Nabe (60) verteilt sind.

2. Walze nach Anspruch 1, dadurch gekennzeichnet, daß der elastomere Oberflächenbelag (50), der diese Fasern enthält, eine Härte von nicht mehr als 75 auf der ASTM D 2240 Type A Durometerskala hat.

3. Walze nach Anspruch 1 oder 2, bei der der elastomere Oberflächenbelag (50) unter Verwendung eines Elastomers ausgebildet wird, der aus der Gruppe ausgewählt ist, die Neopren, Nitril und Urethan umfaßt.

4. Walze nach Anspruch 1, 2 oder 3, bei der der elastomere Verbund, der den elastomeren Oberflächenbelag (50) aufweist, eine Härte zwischen 60 und 70 auf der ASTM D 2240 Type A Durometerskala hat.

5. Walze nach Anspruch 4, bei der die Härte des elastomeren Belages (50) durch Dispersion der Faserstränge (40) auf zwischen 70 und 75 auf der ASTM D 2240 Type A Durometerskala erhöht wird.

6. Walze nach einem der Ansprüche 1—5, bei

der die Länge der Faserstränge (40) nicht größer als 12,7 mm ist.

7. Walze nach Anspruch 6, bei der die Faserstränge (40) auf eine Länge zwischen 4,76 mm und 12,7 mm geschnitten sind.

8. Walze nach einem der Ansprüche 1—7, bei dem die Faserstränge (40) zwischen 0,5 und 3 Gewichtsprozent des Elastomers in dem elastomeren Oberflächenbelag (50) wiegen.

9. Walze nach einem der Ansprüche 1—8, bei dem das Material der Faserstränge ein aromatisches Poliamid, z.B. Kevlar oder Nomex, oder ein Polyäthylen-Terephthalat, z.B. Dacron, aufweist.

10. Walze nach einem der vorausgehenden Ansprüche, bei dem der elastomere Oberflächenbelag (50) durch Klebstoff mit der zylindrischen Nabe (60) verbunden ist.

11. Walze nach einem der Ansprüche 1—10, bei dem der elastomere Belag (50) mit der Nabe (60) unter Wärme- und Druckwirkung verbunden worden ist, um den elastomer Belag auszuhärten.

12. Zugwalzenantriebssystem mit einem Gehäuse (90), einer Walze (80) mit einer zylindrischen Nabe (60), die rotierend antreibbar ist und einen elastomeren Oberflächenbelag (50) besitzt, der sich über die zylindrische äußere Oberfläche der zylindrischen Nabe erstreckt, wobei die Walzennabe im Gehäuse so befestigt ist, daß der elastomere Oberflächenbelag sich zum Teil oberhalb des Pegels des Gehäuses erstreckt, um eine Antriebsoberfläche auszubilden, und einer Vorrhichtung zum selektiv reversierbaren Antrieben der zylindrischen Nabe, dadurch gekennzeichnet, daß der elastomere Oberflächenbelag (50) der Walze in der in einem der Ansprüche 1—11 angegebenen Weise definiert ist.

13. Verfahren zum Herstellen der Zugantriebswalze (80) nach einem der Ansprüche 1—11, dadurch gekennzeichnet, daß geschnittene Faserstränge (40) in einen ungehärteten elastomeren Verbund mit den geschnittenen Fasersträngen in im wesentlichen paralleler Orientierung eingebracht werden, daß mindestens ein Kissen (50) aus dem ungehärteten elastomeren Verbund mit den eingebrachten geschnittenen Fasersträngen in im wesentlichen paralleler Orientierung im Kissen ausgebildet wird, daß das Kissen (50) um mindestens einen Teil des Umfangs einer zylindrischen Nabe (60) angeordnet wird, wobei die geschnittenen Faserstränge (40) in dem Kissen in im wesentlichen in Umfangsrichtung verlaufender Orientierung um die Nabe angeordnet werden, und daß das Kissen (50) um die Nabe (60) in einer Härtepresse (70, 72) mit Wärme und Druck beaufschlagt wird, um den elastomeren Verbund auszuhärten.

14. Verfahren nach Anspruch 13 bei dem der ungehärtete elastomere Verbund auf einer Doppelwalzenmühle (20) gefahren wird, daß die geschnittenen Faserstränge (40) auf den ungehärteten elastomeren Verbund aufgebracht werden, während dieser auf der Doppelrollenmühle (20) gefahren wird, wobei die geschnittenen Faserstränge dadurch in den ungehärteten

elastomeren Verbund mit im wesentlichen paralleler Orientierung eingeführt werden.

15. Verfahren nach Anspruch 13 oder 14, bei dem der ungehärtete elastomere Verbund mit den in den Verbund eingebrachten geschnittenen Fasern (40) zu einer vorgewählten Dicke gevalzt wird und der ungehärtete elastomere Verbund mit den geschnittenen, darin eingebauten geschnittenen Fasern (40) auf eine vorgewählte Dicke geschnitten wird, und der ungehärtete elastomere Verbund mit den darin eingebauten Fasern (40) zu einer vorbestimmten Größe geschnitten wird.

16. Verfahren nach einem der Ansprüche 13—15, bei dem eine Vielzahl derartiger Kissen (50) ausgebildet und um die Nabe (60) herum so angeordnet werden, daß dergesamte Umfang der Nabe bedeckt wird, wobei jedes der Kissen so angeordnet wird, daß die darin enthaltenen geschnittenen Fasern in im wesentlichen in Umfangsrichtung verlaufender Orientierung um die Nabe (60) orientiert werden.

17. Verfahren nach einem der Ansprüche 13—16, bei dem das Aufgeben von Wärme und Druck das Aufgeben eines Druckes von zwischen 4136,856 und 6894,76 kPa bei etwa 154° C über eine Zeitspanne von etwa 35 Minuten erfolgt.

18. Verfahren nach Anspruch 17, bei dem zusätzlich ein Klebstoff auf die Nabe (60) aufgetragen wird, bevor das Kissen um die Nabe herum angeordnet wird.

19. Verfahren zur Herstellung einer Zugantriebswalze, dadurch gekennzeichnet, daß eine zylindrische Nabe (60), die drehbar angetrieben wird, vorgesehen wird, daß eine Vielzahl von Längen von Fasersträngen (40) in einen elastomeren Verbund dispergiert werden, wobei die Faserstränge nur in im wesentlichen paralleler Orientierung angeordnet sind, und daß um die zylindrische Nabe (60) herum ein Belag (50) aus dem elastomeren Verbund angebracht wird, wobei die dispergierten Faserstränge (40) so angeordnet sind, daß die Orientierung der Faserstränge in dem Belag des elastomeren Verbundes im wesentlichen in Umfangsrichtung um die zylindrische Nabe erfolgt.

Revendications

1. Rouleau (80) pour entraînement en traction de charges, comprenant: un moyeu cylindrique (60), prévu pour être entraîné, et une couche de surface en élastomère (50) installée de façon fixe sur ledit moyeu cylindrique pour un contact de traction avec les charges, caractérisé en ce que ladite couche de surface en élastomère (50) contient des filaments de fibres (40) dispersés dans cette couche, seulement suivant une orientation sensiblement circonférentielle autour dudit moyeu cylindrique (60).

2. Rouleau suivant la revendication 1, dans lequel ladite couche de surface en élastomère (50) contenant lesdites fibres a une dureté non supérieure à 75 sur l'échelle de dureté ASTM D 2240 type A.

5 3. Rouleau suivant la revendication 1 ou la revendication 2, dans lequel ladite couche de surface en élastomère (50) est composé à partir d'un élastomère choisi dans le groupe comprenant néoprène, nitrile et uréthane.

10 4. Rouleau suivant la revendication 1 ou la revendication 2 ou la revendication 3, dans lequel le composé élastomère constituant ladite couche de surface en élastomère (50) a une dureté comprise entre 60 et 70 sur l'échelle de dureté ASTM D 2240 type A.

15 5. Rouleau suivant la revendication 4, dans lequel la dureté de la couche d'élastomère (50) est augmentée par dispersion dans cette couche desdits filaments de fibres (40), jusqu'à une valeur comprise entre 70 et 75 sur l'échelle de dureté ASTM D 2240 type A.

20 6. Rouleau suivant l'une quelconque des revendications 1 à 5, dans lequel lesdits filaments de fibres (40) ont une longueur non supérieure à 12,7 mm (0,5 inch).

25 7. Rouleau suivant la revendication 6, dans lequel lesdits filaments de fibres (40) sont coupés de manière à obtenir des fibres dont la longueur est comprise entre 4,76 mm et 12,7 mm (3/16 inch et 0,5 inch).

30 8. Rouleau suivant l'une quelconque des revendications 1 à 7, dans lequel lesdits filaments de fibres (40) représentent, en poids, entre 0,5% et 3% du poids de l'élastomère dans ladite couche de surface en élastomère (50).

35 9. Rouleau suivant l'une quelconque des revendications 1 à 8, dans lequel la matière desdits filaments de fibres est un polyamidé aromatique, par exemple Kevlar ou Nomex, ou un téréphthalate de polyéthylène, par exemple Dacron.

40 10. Rouleau suivant l'une quelconque des revendications précédentes, dans lequel ladite couche de surface en élastomère (50) est liée par un adhésif audit moyeu cylindrique (60).

45 11. Rouleau suivant l'une quelconque des revendications 1 à 10, dans lequel ladit couche en élastomère (50) est liée audit moyeu (60) par application de chaleur et de pression pour durcir ladite couche d'élastomère.

50 12. Système d'entraînement à rouleau de traction, comprenant un carter (90), un rouleau (80) comportant un moyeu cylindrique (60) prévu pour être entraîné en rotation et qui présente une couche de surface en élastomère (50) s'étendant sur la surface extérieure cylindrique dudit moyeu cylindrique, le moyeu de rouleau étant maintenu dans le carter de sorte que ladite couche de surface en élastomère (50) s'étende partiellement au-dessus du niveau dudit carter pour constituer une surface d'entraînement, et des moyens pour entraîner réversiblement de façon sélective ledit moyeu cylindrique, caractérisé en ce que la couche de surface en élastomère (50) du rouleau est comme définie dans l'une quelconque des revendications 1 à 11.

55 60 65 13. Procédé de fabrication du rouleau d'entraînement en traction (80) suivant l'une quelconque des revendications 1 à 11, caractérisé par les opérations de: incorporation de filaments de

fibres coupés (40) dans un composé élastomère non durci, lesdits filaments d'fibres coupés étant orientés sensiblement parallèlement; formation d'au moins un coussinet (50) à partir dudit composé élastomère non durci dans lequel sont incorporés lesdits filaments de fibres coupés (40) dans ladite orientation sensiblement parallèle dans ledit coussinet; mise en place dudit coussinet (50) autour d'au moins une partie de la circonférence d'un moyeu cylindrique (60) de sorte que lesdits filaments de fibres coupés (40) dans ledit coussinet sont orientés sensiblement circonférentiellement autour dudit moyeu; et application de chaleur et de pression audit coussinet (50) autour dudit moyeu (60) dans une presse de cuisson (70, 72) pour durcir ledit composé élastomère.

14. Procédé suivant la revendication 13, dans lequel ladite opération d'incorporation comprend: le passage dudit composé élastomère non durci dans un malaxeur à deux cylindres (20); et la distribution répartie desdits filaments de fibres coupés (40) sur ledit composé élastomère non durci, pendant son passage dans ledit malaxeur à deux cylindres (20), de sorte que lesdits filaments de fibres coupés s'incorporent ainsi dans ledit composé élastomère non durci suivant ladite orientation sensiblement parallèle.

15. Procédé suivant la revendication 13 ou la revendication 14, dans lequel ladite opération de formation comprend: le laminage dudit composé élastomère non durci, dans lequel sont incorporées lesdites fibres coupées (40), jusqu'à une épaisseur prédéterminée; et la coupe dudit composé élastomère non durci, dans lequel sont incorporées lesdites fibres coupées (40), à une

dimension prédéterminée.

16. Procédé suivant l'un quelconque des revendications 13 à 15, dans lequel une pluralité desdits coussinets (50) sont formés et placés autour dudit moyeu (60) de manière à recouvrir toute la circonférence dudit moyeu, chacun desdits coussinets étant placé de sorte que lesdites fibres coupées (40) qui y sont incorporées sont orientées dans ladite orientation sensiblement circonférentielle autour dudit moyeu (60).

17. Procédé suivant l'une quelconque des revendications 13 à 16, dans lequel ladite application de chaleur et de pression comprend l'application d'une pression de 4136,856 à 6894, 76 kPa (600 à 1000 psi) à une température de 154°C (310°F) environ pendant 35 minutes environ.

18. Procédé suivant la revendication 17, comprenant l'opération supplémentaire d'application d'un adhésif audit moyeu (60) avant de placer ledit coussinet autour dudit moyeu.

19. Procédé de fabrication d'un rouleau d'entraînement par traction, caractérisé par les opérations de: préparation d'un moyeu cylindrique (60) prévu pour être entraîné en rotation; dispersion d'une pluralité de tronçons de filaments de fibres (40) dans un composé élastomère de sorte que lesdits filaments de fibres sont orientés seulement sensiblement parallèlement; et installation, autour dudit moyeu cylindrique (60), d'une couche (50) dudit composé élastomère contenant lesdits filaments de fibres dispersés (40) de sorte que l'orientation desdits filaments de fibres dans ladite couche de composé élastomère est sensiblement circonférentielle autour dudit moyeu cylindrique.

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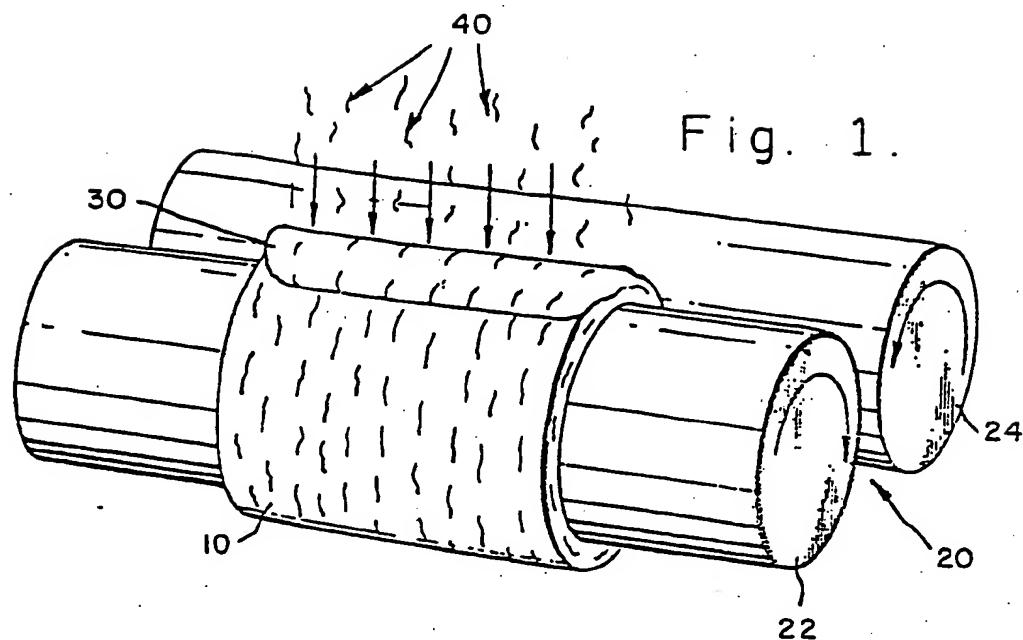
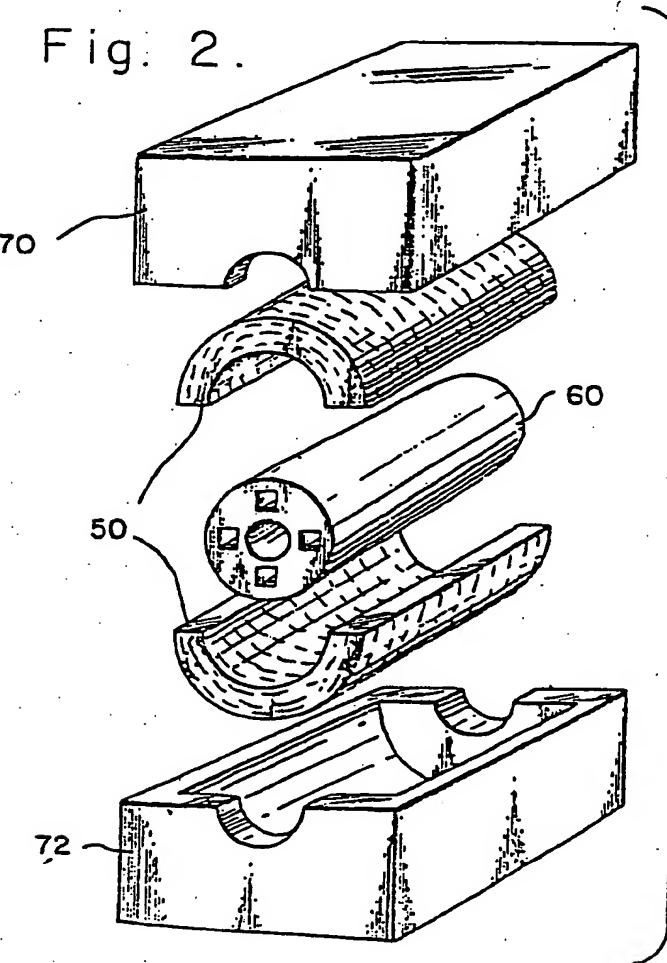


Fig. 2.



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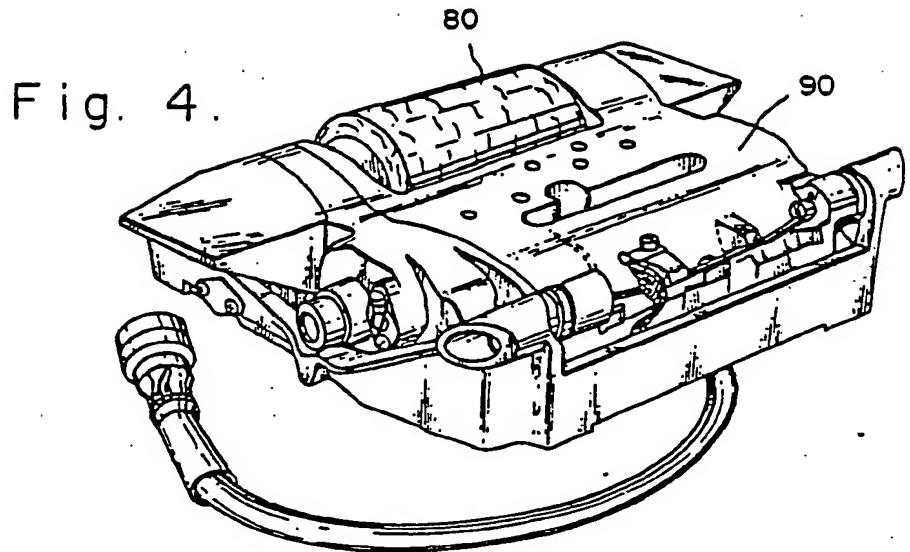


Fig. 3.

